

CHARACTERISTICS OF SYNCHRONOUS/PERMANENT MAGNET HYBRID AC MACHINE

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***Abstract:** This work describes the synchronous/permanent magnet machine. It is shown that the machine has good power density and efficiency, and that the machine has true field regulation capability. The principle of operation, finite element analysis and simulation of this machine are investigated in this work.*

1. INTRODUCTION

In this work is presented a new electric machine named the magnet hybrid (SynPM Hybrid) machine. This machine is a combination of a synchronous/permanent machine (PM) and a wound field synchronous machine. It has both PM poles and excitation poles on the rotor, retaining the conventional multi-phase machine stator winding. It has both the features of both PM and synchronous machines. The PM poles provide the air gap with major part of air gap flux. The excitation poles act as the flux regulator to adjust the air gap flux distribution. By proper connection the of stator windings, field weakening/strengthening operation is achieved by picking up the electromotive force (emf) changes caused by the change of flux density under the excitation poles. Although the slip rings and brushes are still present in this kind of electric machine, failure of the brush rigging will not cause as severe a problem as it would for the conventional wound field synchronous machine since the PM poles still produce fairly large air gap flux even with the field winding out of service.

2. PRINCIPLE OF OPERATION

The structure of the SynPM machine is shown in Figure. 1. The machine has six poles in which 4 of the rotor poles are PM poles and the remaining 2 poles are excitation poles. In general, the operation of this type of machines is quite similar to that of the permanent magnet synchronous machine except that this new structure possesses field regulation characteristics. For easy understanding of the operation principle, an ideal magnetic circuit analysis is helpful. In this analysis, the following points are assumed: 1) The iron has infinite permeance; 2) Fringing and leakage fluxes are neglected; 3) Even distribution of flux under a pole and 4) Even distribution of flux in the region between poles; 5) Smooth surfaces on both stator bore and rotor poles. Based on the above assumption and "Norton" equivalent circuit for magnet [1], a magnetic circuit model of SynPM machine can be constructed and is shown in Figure 2. The circuit model has two rings, representing stator core and rotor core, twelve magnetic reluctances, and six magnetomotive force (mmf) sources. In this model R_g is the air gap reluctance of the excitation poles R_{pm} is the reluctance of the PM poles and R_s is the reluctance of the slot between two poles. F_{ex} is the mmf of the field winding of excitation pole.

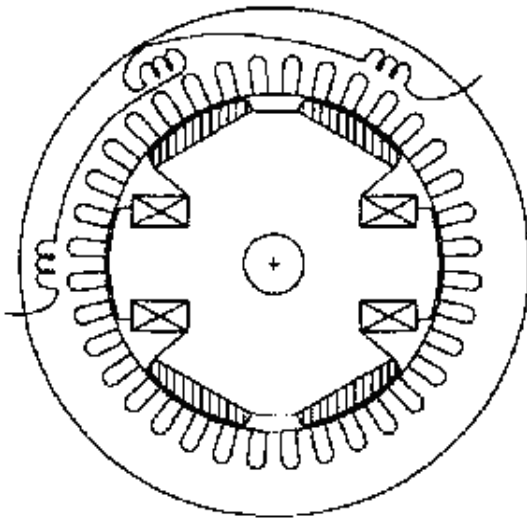


Figure 1. Structures of SynPM Machine.

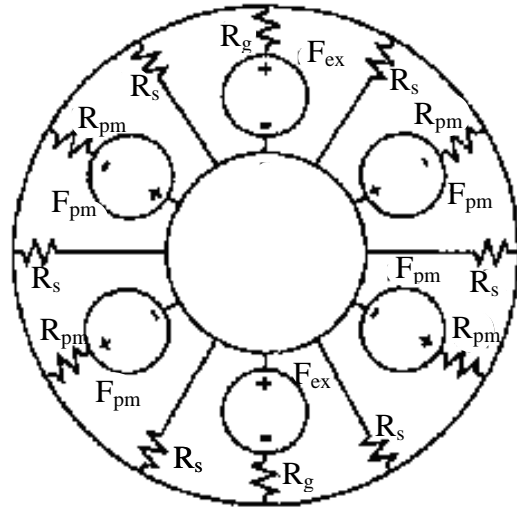


Figure 2. Magnetic Circuit of 6 pole SynPM Machine.

The circuit is described by the following equation:

$$\sum_{i=1}^{12} \frac{1}{R_i} \cdot P = \sum_{i=1}^{12} \frac{F_i}{R_i} , \quad (1)$$

where P is the magnetic potential of the rotor core (taking stator core as zero reference), F_i is the mmf of branch i , R_i is the reluctance of the branch i . Since the magnets and field windings are present in pairs and thus cancel each other, $\sum_{i=1}^{12} \frac{F_i}{R_i}$ is always zero. From equation (1);

$$P=0 \quad (2)$$

Thus the flux of a branch i is:

$$\Phi_i = \frac{1}{R_i} \cdot F_i, \quad (3)$$

the flux of an excitation pole is

$$\Phi_{ex} = \frac{F_{ex}}{R_g} \quad (4)$$

and the flux of a PM pole is

$$\Phi_{pm} = \frac{F_{pm}}{R_{pm}} . \quad (5)$$

From equation (4) it is apparent that changing F_{ex} can easily change the flux of the excitation poles, since the air gap reluctance R_g is normally very small. However, the flux of

the PM pole is difficult to change due to the typically large value of reluctance R_{pm} . When field current changes, it can change the back emf of a circuit, assuming that speed is maintained constant. Figure 1 shows an example of the connection.

3. COUPLED CIRCUIT SIMULATION

A magnetic circuit analysis is used to calculate the parameters for coupled circuit simulation [2] [3]. Figure 3 shows the calculated circuit self inductance versus rotor angular

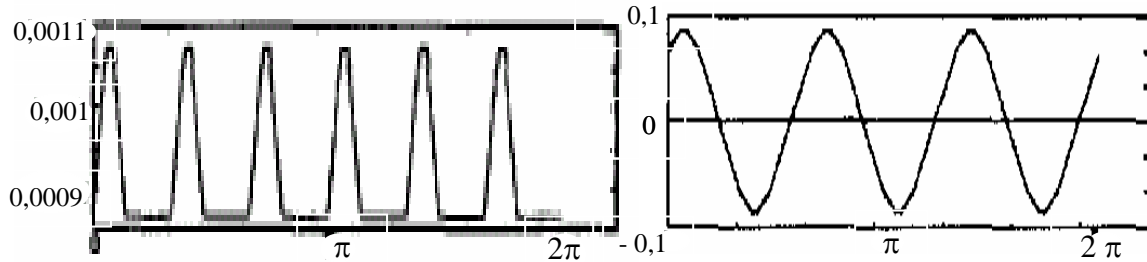


Figure 3. Calculated Circuit Inductances.

Figure 4. Calculated Flux Linkages of One Circuit.

position curve. There are six positions where the inductance reaches its maximum as a result of the series connection of the member coils of the circuit. The flux linkage of circuits produced by PM poles is another important issue in the simulation. The circuit flux linkage can also be calculated by magnetic circuit analysis [4] and is shown in Figure 4. From the curve it is clear that from the terminals of the circuit, the number of poles is six, which is achieved by connecting the coils of same phase under all poles in series. A simulation study has been made to determine the performance of the SynPM machine. From simulations, it should be clear that the SynPM machine with field current regulation capability has much higher constant power speed range with considerably improved torque capability than an equivalent PM machine.

4. FINITE ELEMENT (FEM) ANALYSIS

To verify the results of the ideal magnetic circuit analysis, an FEM analysis was also conducted. Figure 5 shows the flux lines of the SynPM machine with positive field current. Figure 6 shows another case of the SynPM machine with zero fields current, and, finally, Figure 7 shows the case where the field current is negative, or the field weakening case. From these FEM resulting plots it is apparent that a change of field current does indeed change the flux pattern in the SynPM machine as predicted.

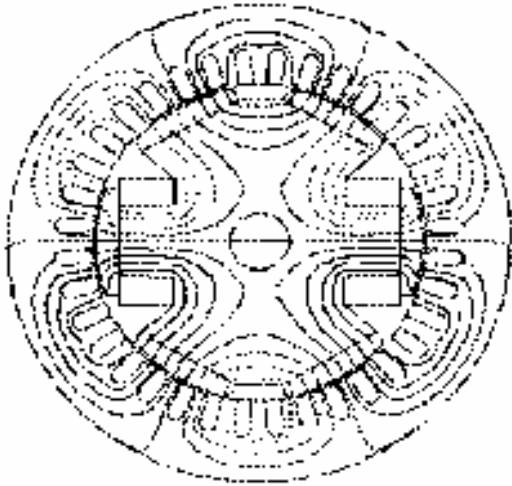


Figure 5. Flux lines of 6 Pole SynPM machine with Full Positive Field Current.

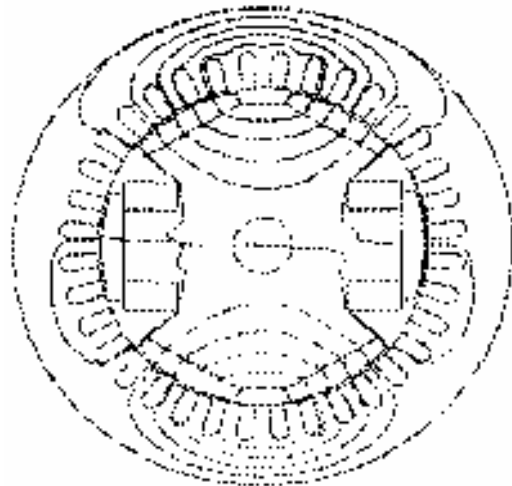


Figure 6. Flux lines of 6 Pole SynPM machine with Zero Field Current.

5. CONCLUSIONS

The synchronous/permanent magnet hybrid machine (SynPM Hybrid) can work as a generator or a motor. Although a 6 pole version is discussed here, an 8 pole version functions in a similar manner with 4 PM poles and 4 excitation poles. The SynPM machine has true field regulation. The machine can operate at high speed with field weakening capability. It has potentials of achieving high efficiency and high power density due to the use of PM material. The ability to operate as pure PM machine increases its reliability. However, the slip ring and brushes are still present. Also there is high flux density present in the stator core region between two adjacent PM poles at high speed when weakening the field,

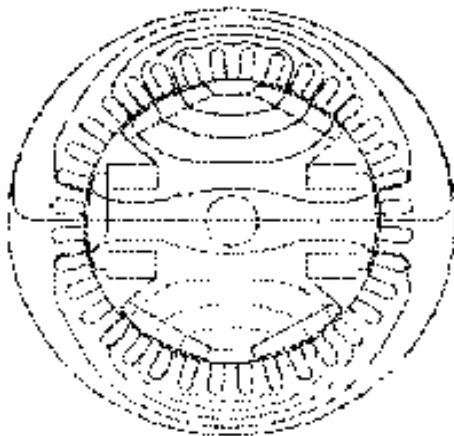


Figure 7. Flux lines of 6 Pole SynPM machine with full Negative Field Current.

which may cause high iron loss in the stator core. Considering the gains in power density, efficiency and reliability, it can be concluded that the SynPM drive has potential to compete with conventional AC induction motor drives in higher horsepower applications where the added cost of the rotor structure is offset by the improvement gains in size and weight of the machine and by reduced cost in the power converter.

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